

Providing Safe Schools for Our Students

by

Timothy J. Walsh

Washington Department of Natural
Resources

Division of Geology and Earth Resources

October 25, 2011



WASHINGTON STATE DEPARTMENT OF
Natural Resources



“Children have the right to be safe in school buildings during earthquakes”

-Western States Seismic Policy Council

WASHINGTON STATE SCHOOL SEISMIC SAFETY PILOT PROJECT— Providing Safe Schools for Our Students



by the Washington State Seismic Safety Committee



Washington Military Department
Emergency Management Division



WASHINGTON STATE DEPARTMENT OF
Natural Resources
Peter Goldmark • Commissioner of Public Lands

Why Assess School Buildings?

- Do YOU know how many schools in Washington State are vulnerable to extensive damage or even collapse in an earthquake?
- Do YOU know how many kids are at risk in these buildings?
- Do YOU know which school districts have retrofitted some or all their buildings?
- **You might be surprised to know that neither does anyone else...**
- With a critical shortfall of already scarce financial resources (e.g.. Trust lands funding) available to build or retrofit, how can state & local decision makers best prioritize actions and know where to put these resources?



Washington Schools have been Damaged in Earthquakes

1949, a large earthquake collapsed the gymnasium roof at Puyallup High School. The earthquake occurred at 11:58 a.m., and the gym had just been vacated by workers for lunch.

At Castle Rock High School, however, falling masonry killed the student body president as he tried to escape from the building.

Another student was killed by falling bricks at Lowell Grammar School in Tacoma

In all, thirty schools were damaged in this Nisqually-type earthquake



Figure 2. At Castle Rock, a high school student was killed as unanchored gable masonry cascaded to the walk outside the entrance. There could have been more casualties. (From Edwards, 1951.)



Figure 1. Open air theatre—Three members of the stage crew at Puyallup High School survey the wreckage of the stage, which was caved in by the earthquake just as they were leaving for lunch. Under the debris are a ping-pong table and a grand piano. Seattle Times staff photo by Larry Dion (from Ulrich, 1949).



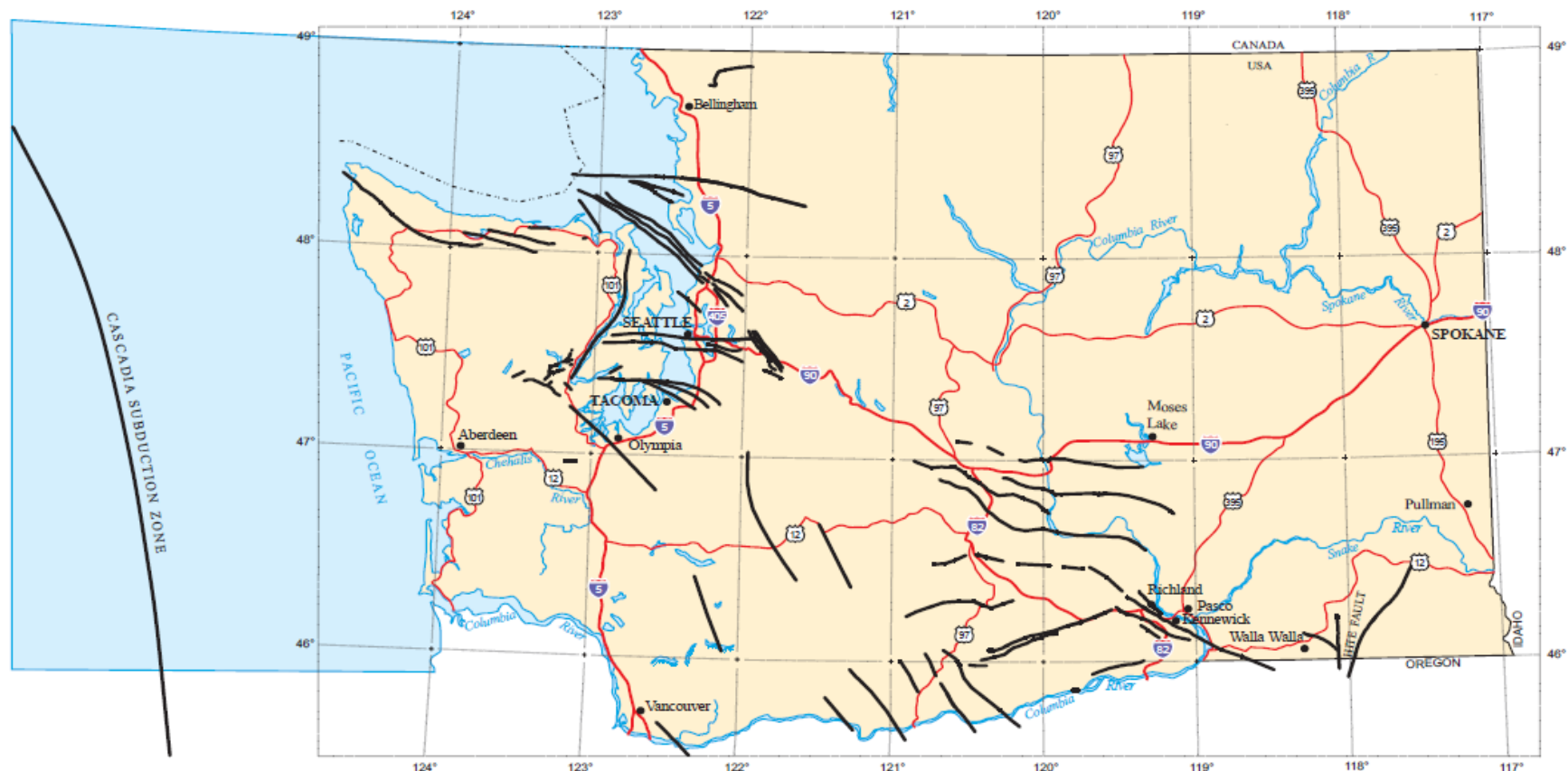
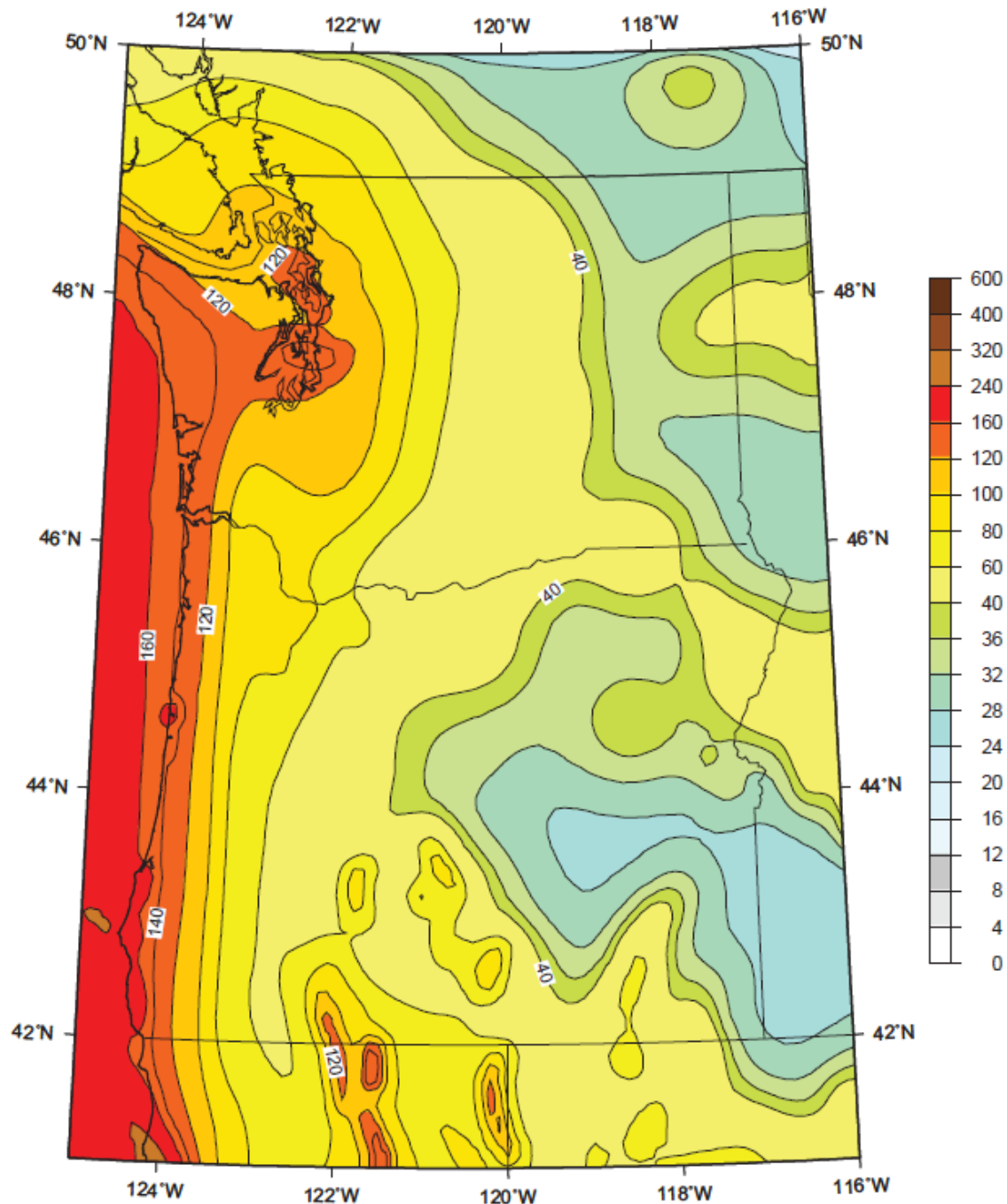


Figure 3. Simplified map of known and suspected active faults (heavy black lines) affecting earthquake hazard in Washington. It includes faults that have been demonstrated to have caused earthquakes since the last ice age but also faults that are under investigation.

What are the sources of earthquakes in Washington? Here are the active and suspected active faults in Washington



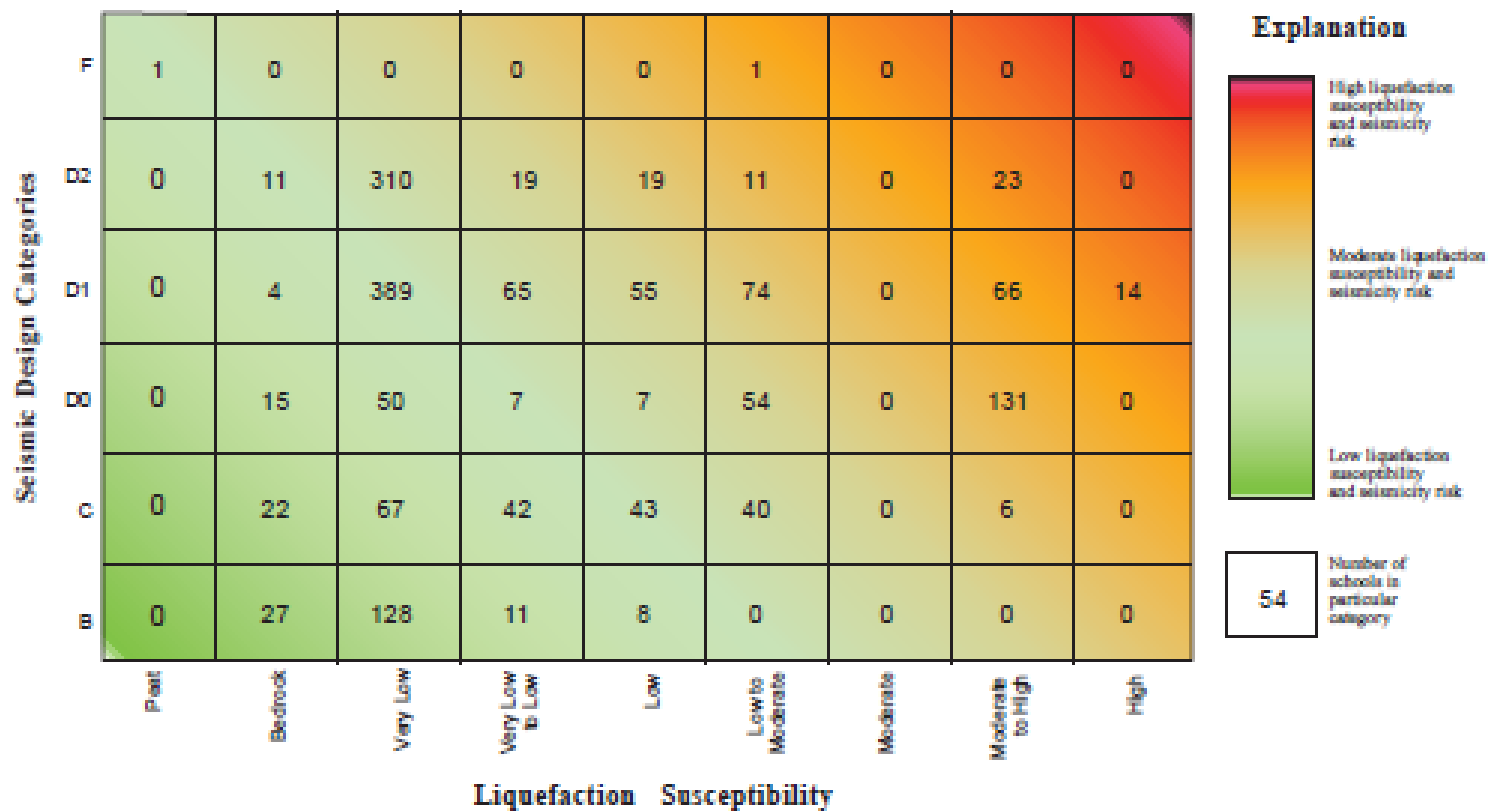
Probabilistic
seismic hazard
map for the
Pacific
Northwest. This
is the basis of
the 2009
International
Building Code



Selection Process

- 1) Our initial screening was to consider school districts that had high earthquake hazard. We mapped schools on a combination of the seismic design category map and liquefaction susceptibility maps.
- 2) School districts in both eastern and western Washington that scored high in criterion 1 were plotted.
- 3) The number of schools per district were considered, both to equalize each district and to select a number of school buildings that could be evaluated with the available resources.
- 4) A representative of the Office of the Superintendent of Public Instruction then contacted a select number of school districts to determine their willingness to participate.

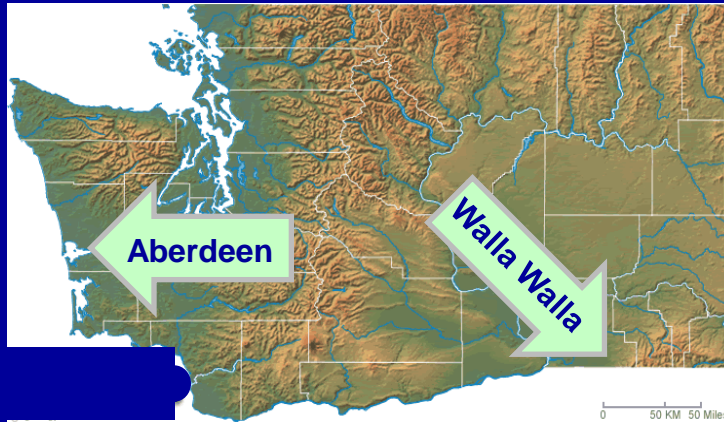




Note: The seismic design category combines an estimate of the strength of ground shaking at any individual site with the amplification caused by the local geology.

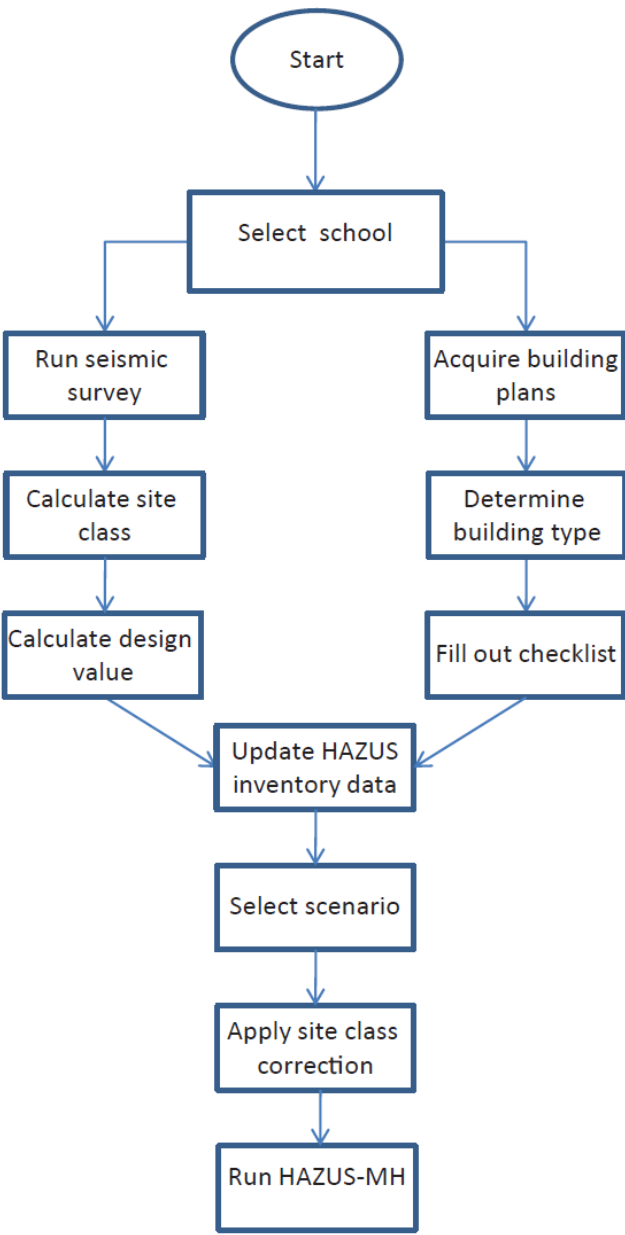


School Seismic Needs Assessment



- Pilot Project in the Cities of Walla Walla and Aberdeen
- Leverage volunteer expertise from Structural Engineering Association of Washington (SEAW) to investigate structural issues and Washington Association of Building Officials (WABO) to evaluate non-structural issues.
- Project used ASCE 31: Evaluation of Existing Buildings for structural assessment, VS-30 data for local geology assessment, and HAZUS for modeling of potential losses using 2 different scenarios.
- Intent was to develop a method that can be used statewide to assess all school buildings for seismic safety.





Screening Process



Aberdeen administration building





Building Name: Administration Building

Date: 11/15/10

Building Address: 216 N 'G' Street, Aberdeen, WA 98520

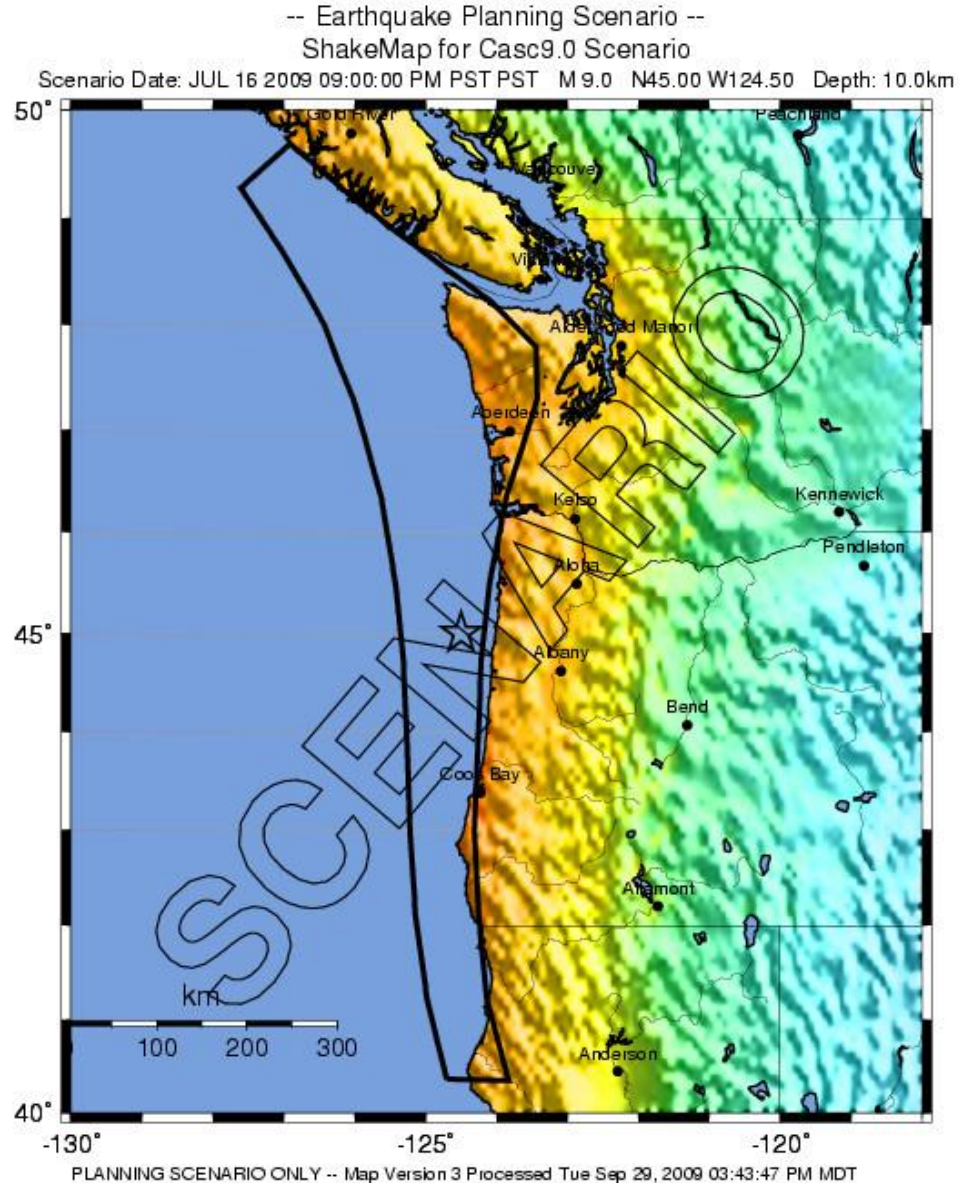
Page: 1 of

Job Number: Job Name: By: MEB Checked:

ASCE 31 BASIC CHECKLIST URMA: UNREINFORCED MASONRY BEARING WALL BUILDINGS WITH RIGID OR STIFF DIAPHRAGMS





| C | NC | N/A | | | Comments |
|-------------------------------------|-------------------------------------|--------------------------|---------|--|---|
| BUILDING SYSTEM | | | | | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.1.1 | LOAD PATH: The structure shall contain a minimum of one complete load path for Life Safety and Immediate Occupancy for seismic force effects from any horizontal direction that serves to transfer the inertial forces from the mass to the foundation. | Diaphragms-to-walls; walls-to-foundation. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.1.3 | MEZZANINES: Interior mezzanine levels shall be braced independently from the main structure, or shall be anchored to the lateral-force-resisting elements of the main structure. | Mezzanine attached to main LFERS. |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | 4.3.2.1 | WEAK STORY: The strength of the lateral-force-resisting system in any story shall not be less than 80% of the strength in an adjacent story, above or below, for Life-Safety and Immediate Occupancy. | Top Flr, N-S Direction, Approx 66% of 1 st Flr |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | 4.3.2.2 | SOFT STORY: The stiffness of the lateral-force-resisting system in any story shall not be less than 70% of the lateral-force-resisting system stiffness in an adjacent story above or below, or less than 80% of the average lateral-force-resisting system stiffness of the three stories above or below for Life Safety and Immediate Occupancy. | 1 st Flr, E-W Direction, Approx 44% of Top Flr |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | 4.3.2.3 | GEOMETRY: There shall be no changes in horizontal dimension of the lateral-force-resisting system of more than 30% in a story relative to adjacent stories for Life Safety and Immediate Occupancy, excluding one-story penthouses and mezzanines. | Lower portion of building is > 30% length of upper portion. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.2.4 | VERTICAL DISCONTINUITIES: All vertical elements in the lateral-force-resisting system shall be continuous to the foundation. | All vertical elements continuous to foundation. |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | 4.3.2.5 | MASS: There shall be no change in effective mass of more than 50% from one story to the next for Life Safety and Immediate Occupancy. Light roofs, penthouses and mezzanines need not be considered. | Roof Approx 30% Wt of combined 2 nd Flr/Lower Bldg Roof. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.2.6 | TORSION: The estimated distance between the story center of mass and the story center of rigidity shall be less than 20% of the building width in either plan dimension for Life Safety and Immediate Occupancy. | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.3.4 | DETERIORATION OF CONCRETE: There shall be no visible deterioration of concrete or reinforcing steel in any of the vertical- or lateral-force-resisting elements. | No significant deterioration observed. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.3.7 | MASONRY UNITS: There shall be no visible deterioration of masonry units. | No significant deterioration observed. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.3.8 | MASONRY JOINTS: The mortar shall not be easily scraped away from the joints by hand with a metal tool, and there shall be no areas of eroded mortar. | Mortar was sound. |

Scenario Magnitude 9.0 earthquake on the Cascadia subduction zone (from Art Frankel)



| PERCEIVED SHAKING | Not felt | Weak | Light | Moderate | Strong | Very strong | Severe | Violent | Extreme |
|------------------------|----------|---------|---------|------------|--------|-------------|----------------|---------|------------|
| POTENTIAL DAMAGE | none | none | none | Very light | Light | Moderate | Moderate/Heavy | Heavy | Very Heavy |
| PEAK ACC. (%g) | <.17 | .17-1.4 | 1.4-3.9 | 3.9-9.2 | 9.2-18 | 18-34 | 34-65 | 65-124 | >124 |
| PEAK VEL. (cm/s) | <0.1 | 0.1-1.1 | 1.1-3.4 | 3.4-8.1 | 8.1-16 | 16-31 | 31-60 | 60-116 | >116 |
| INSTRUMENTAL INTENSITY | I | II-III | IV | V | VI | VII | VIII | IX | X+ |



| Damage state | | Description |
|--|-----------|---|
|  | Slight | Small plaster cracks at corners of door and window openings and wall-ceiling intersections; small cracks in masonry chimneys and masonry veneers. Small cracks are assumed to be visible with a maximum width of less than 1/8 inch (cracks wider than 1/8 inch are referred to as "large" cracks). |
|  | Moderate | Large plaster or gypsum-board cracks at corners of door and window openings; small diagonal cracks across shear-wall panels exhibited by small cracks in stucco and gypsum wall panels; large cracks in brick chimneys; toppling of tall masonry chimneys. |
|  | Extensive | Large diagonal cracks across shear-wall panels or large cracks at plywood joints; permanent lateral movement of floors and roof; toppling of most brick chimneys; cracks in foundations; splitting of wood sill plates and/or slippage of structure over foundations. |
|  | Complete | Structure may have large permanent lateral displacement or be in imminent danger of collapse due to cripple-wall failure or failure of the lateral-load-resisting system; some structures may slip and fall off the foundation; large foundation cracks. Three percent of the total area of buildings with Complete damage is expected to be collapsed, on average. |



Aberdeen, Building Code Value

| Name | None | Slight | Moderate | Extensive | Complete | At Least Extensive |
|-------------------------------|------|--------|----------|-----------|----------|--------------------|
| A J WEST ELEMENTARY | 15% | 56% | 28% | 1% | 0% | 1% |
| ABERDEEN S DIST ADMIN BLD | 0% | 0% | 0% | 2% | 98% | 100% |
| ALEXANDER YOUNG ELEM | 0% | 0% | 0% | 8% | 92% | 100% |
| CENTRAL PARK ELEMENTARY | 0% | 1% | 28% | 54% | 17% | 72% |
| HARBOR HIGH SCHOOL | 0% | 0% | 0% | 8% | 92% | 100% |
| HOPKINS ELEMENTARY | 0% | 0% | 0% | 8% | 92% | 100% |
| J M WEATHERWAX - ABERDEEN HS | 41% | 45% | 13% | 0% | 0% | 0% |
| MCDERMOTH ELEMENTARY | 45% | 42% | 13% | 0% | 0% | 0% |
| MILLER JUNIOR HIGH | 0% | 0% | 5% | 42% | 53% | 95% |
| ROBERT GRAY ELEMENTARY | 54% | 41% | 5% | 0% | 0% | 0% |
| SAM BENN GYM (ABERDEEN HS) | 34% | 54% | 12% | 0% | 0% | 0% |
| STEVENS ELEMENTARY SCHOOL | 0% | 0% | 5% | 42% | 53% | 95% |
| STEWART BLD - ROBERT GRAY ELM | 0% | 0% | 3% | 32% | 66% | 97% |



Aberdeen, M9.0 scenario

| Name | None | Slight | Moderate | Extensive | Complete | At Least Extensive |
|--------------------------------|------|--------|----------|-----------|----------|--------------------|
| SAM BENN GYM (ABERDEEN HS) | 4% | 40% | 53% | 4% | 0% | 4% |
| STEWART BUILDING (Robert Gray) | 0% | 1% | 17% | 56% | 26% | 82% |
| ROBERT GRAY ELEMENTARY | 2% | 34% | 58% | 6% | 0% | 6% |
| A J WEST ELEMENTARY | 4% | 40% | 53% | 4% | 0% | 4% |
| ALEXANDER YOUNG ELEMENTARY | 0% | 1% | 24% | 56% | 18% | 74% |
| ABERDEEN S. DIST ADMIN BLD. | 0% | 1% | 10% | 38% | 51% | 90% |
| CENTRAL PARK ELEMENTARY | 1% | 22% | 67% | 10% | 0% | 10% |
| HARBOR HIGH SCHOOL | 0% | 1% | 24% | 56% | 18% | 74% |
| HOPKINS ELEMENTARY | 0% | 1% | 24% | 56% | 18% | 74% |
| J M WEATHERWAX (ABERDEEN) HS | 13% | 44% | 41% | 2% | 0% | 2% |
| MCDERMOTH ELEMENTARY | 2% | 20% | 59% | 19% | 0% | 19% |
| MILLER JUNIOR HIGH | 0% | 9% | 65% | 24% | 2% | 26% |
| STEVENS ELEMENTARY SCHOOL | 0% | 9% | 65% | 24% | 2% | 26% |



Green Park Elementary





Building Name: Green Park Elementary – Original Building

Date: _____

Building Address: _____

Page: 1 of 2

Job Number: _____

Job Name: _____

By: DRW Checked: _____

ASCE 31 BASIC CHECKLIST URM: UNREINFORCED MASONRY BEARING WALL BUILDINGS WITH FLEXIBLE DIAPHRAGMS

| C | NC | N/A | | Comments |
|-------------------------------------|-------------------------------------|-------------------------------------|---------|--|
| BUILDING SYSTEM | | | | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.1.1 | LOAD PATH: The structure shall contain a minimum of one complete load path for Life Safety and Immediate Occupancy for seismic force effects from any horizontal direction that serves to transfer the inertial forces from the mass to the foundation. |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | 4.3.1.2 | ADJACENT BUILDINGS: The clear distance between the building being evaluated and any adjacent building shall be greater than 4% of the height of the shorter building for Life Safety and Immediate Occupancy. 2" seismic joint provided. Attic is 44.5 ft AFF, requiring a 21" seismic separation. |
| <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | 4.3.1.3 | MEZZANINES: Interior mezzanine levels shall be braced independently from the main structure, or shall be anchored to the lateral-force-resisting elements of the main structure. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.2.1 | WEAK STORY: The strength of the lateral-force-resisting system in any story shall not be less than 80% of the strength in an adjacent story, above or below, for Life-Safety and Immediate Occupancy. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.2.2 | SOFT STORY: The stiffness of the lateral-force-resisting system in any story shall not be less than 70% of the lateral-force-resisting system stiffness in an adjacent story above or below, or less than 80% of the average lateral-force-resisting system stiffness of the three stories above or below for Life Safety and Immediate Occupancy. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.2.3 | GEOMETRY: There shall be no changes in horizontal dimension of the lateral-force-resisting system of more than 30% in a story relative to adjacent stories for Life Safety and Immediate Occupancy, excluding one-story penthouses and mezzanines. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.2.4 | VERTICAL DISCONTINUITIES: All vertical elements in the lateral-force-resisting system shall be continuous to the foundation. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.2.5 | MASS: There shall be no change in effective mass of more than 50% from one story to the next for Life Safety and Immediate Occupancy. Light roofs, penthouses and mezzanines need not be considered. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.3.1 | DETERIORATION OF WOOD: There shall be no signs of decay, shrinkage, splitting, fire damage, or sagging in any of the wood members and none of the metal connection hardware shall be deteriorated, broken, or loose. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.3.7 | MASONRY UNITS: There shall be no visible deterioration of masonry units. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.3.8 | MASONRY JOINTS: The mortar shall not be easily scraped away from the joints by hand with a metal tool, and there shall be no areas of eroded mortar. Limited assessment made of joints. |

Building Name: Green Park Elementary – Original Building

Date: _____

Building Address: _____ Page: 2 of 2Job Number: _____ Job Name: _____ By: DRW Checked: _____**ASCE 31 BASIC CHECKLIST URM: UNREINFORCED MASONRY BEARING WALL
BUILDINGS WITH FLEXIBLE DIAPHRAGMS**

| C | NC | N/A | | Comments |
|---------------------------------------|-------------------------------------|-------------------------------------|-----------|---|
| BUILDING SYSTEM | | | | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.3.3.11 | UNREINFORCED MASONRY WALL CRACKS: There shall be no existing diagonal cracks in the wall elements greater than 1/8" for Life Safety and 1/16" for Immediate Occupancy, or out-of-plane offsets in the bed joint greater than 1/8" for Life Safety and 1/16" for Immediate Occupancy, and shall not form an X pattern. |
| LATERAL-FORCE-RESISTING SYSTEM | | | | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.4.2.1.1 | REDUNDANCY: The number of lines of shear walls in each principal direction shall be greater than or equal to 2 for Life Safety and Immediate Occupancy. |
| <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | 4.4.2.5.1 | SHEAR STRESS CHECK: The shear stress in the unreinforced masonry shear walls, calculated using the Quick Check procedure of Section 3.5.3.3, shall be less than 30 psi for clay units and 70 psi for concrete units for Life Safety and Immediate Occupancy. |
| CONNECTIONS | | | | |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | 4.6.1.1 | WALL ANCHORAGE: Exterior concrete or masonry walls, that are dependent on the diaphragm for lateral support, shall be anchored for out-of-plane forces at each diaphragm level with steel anchors, reinforcing dowels, or straps that are developed into the diaphragm. Connections shall have adequate strength to resist the connection force calculated in the Quick Check Procedure of Section 3.5.3.7. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.6.1.2 | WOOD LEDGERS: The connection between the wall panels and the diaphragm shall not induce cross-grain bending or tension in the wood ledgers. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | 4.6.2.1 | TRANSFER TO SHEAR WALLS: Diaphragms shall be connected for transfer of loads to the shear walls for Life Safety and the connections shall be able to develop the lesser of the shear strength of the walls or diaphragms for Immediate Occupancy. |
| <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | 4.6.4.1 | GIRDER/COLUMN CONNECTION: There shall be a positive connection utilizing plates, connection hardware, or straps between the girder and the column support. |

Not evaluated due to retrofit with SCBF's.

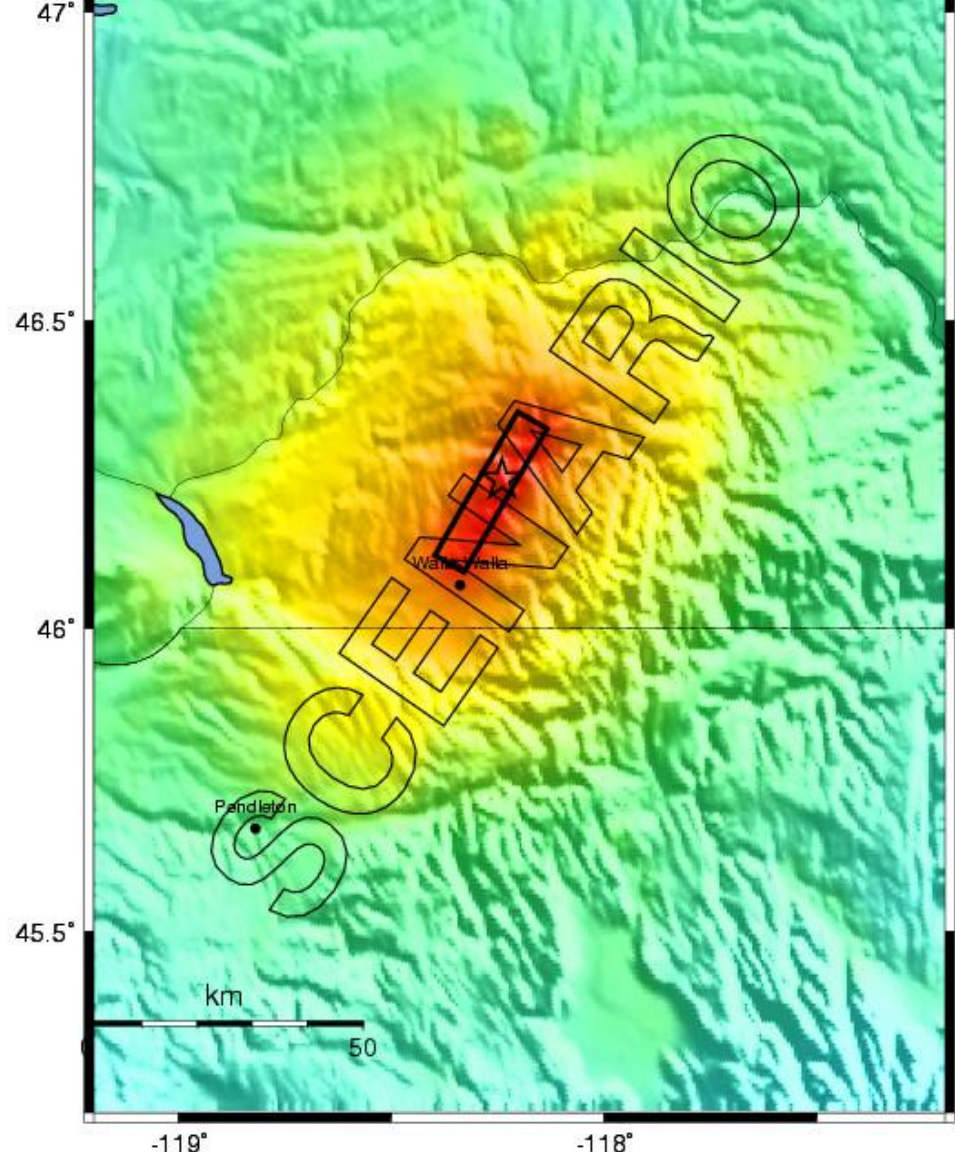
See details 4 and 5 on Sheet S5.2

See details 4 and 5 on Sheet S5.2

Floor joists span between bearing walls only.

Scenario

Magnitude 6.7 earthquake on the Hite fault, scaled up from the 1936 Milton-Freewater earthquake (from Art Frankel)



PLANNING SCENARIO ONLY -- Map Version 2 Processed Wed Aug 4, 2010 04:57:21 PM MDT

| PERCEIVED SHAKING | Not felt | Weak | Light | Moderate | Strong | Very strong | Severe | Violent | Extreme |
|------------------------|----------|---------|---------|------------|--------|-------------|----------------|---------|------------|
| POTENTIAL DAMAGE | none | none | none | Very light | Light | Moderate | Moderate/Heavy | Heavy | Very Heavy |
| PEAK ACC. (%g) | <.17 | .17-1.4 | 1.4-3.9 | 3.9-9.2 | 9.2-18 | 18-34 | 34-65 | 65-124 | >124 |
| PEAK VEL. (cm/s) | <0.1 | 0.1-1.1 | 1.1-3.4 | 3.4-8.1 | 8.1-16 | 16-31 | 31-60 | 60-116 | >116 |
| INSTRUMENTAL INTENSITY | I | II-III | IV | V | VI | VII | VIII | IX | X+ |



Walla Walla, Building Code Value

| Name | None | Slight | Moderate | Extensive | Complete | At least extensive |
|-----------------------------|------|--------|----------|-----------|----------|--------------------|
| BERNEY ELEM | 53% | 22% | 20% | 4% | 1% | 5% |
| BERNEY ELEM GYM | 53% | 22% | 20% | 4% | 1% | 5% |
| BLUE RIDGE ELEM | 62% | 24% | 12% | 2% | 0% | 2% |
| EDISON ELEM | 61% | 20% | 16% | 3% | 0% | 3% |
| GARRISON MIDDLE S | 64% | 26% | 9% | 1% | 0% | 1% |
| GREEN PRK ELEM_additional | 64% | 26% | 9% | 1% | 0% | 1% |
| GREEN PRK ELEM_original | 39% | 26% | 24% | 9% | 2% | 11% |
| LINCOLN ALTERNTV HS | 39% | 26% | 24% | 9% | 2% | 11% |
| PAINE CAMPUS | 62% | 27% | 10% | 1% | 0% | 1% |
| PIONEER MIDDLE | 64% | 26% | 9% | 1% | 0% | 1% |
| PROSPECT POINT ELM | 29% | 15% | 31% | 22% | 3% | 25% |
| SHARPSTEIN (Gym and Lunch) | 69% | 16% | 13% | 3% | 0% | 3% |
| SHARPSTEIN ELEM S | 51% | 28% | 19% | 1% | 0% | 1% |
| WALLA WALLA HS (Academic) | 61% | 18% | 17% | 4% | 0% | 4% |
| WALLA WALLA HS (Auditorium) | 42% | 26% | 28% | 4% | 0% | 4% |
| WALLA WALLA HS (Commons) | 29% | 15% | 31% | 22% | 3% | 25% |
| WALLA WALLA HS (Large Gym) | 61% | 18% | 17% | 4% | 0% | 4% |
| WALLA WALLA HS (Library) | 48% | 23% | 24% | 5% | 1% | 6% |
| WALLA WALLA HS (Music) | 32% | 21% | 36% | 9% | 2% | 11% |
| WALLA WALLA HS(Science) | 29% | 15% | 31% | 22% | 3% | 25% |
| WALLA WALLA HS (Small Gym) | 29% | 15% | 31% | 22% | 3% | 25% |
| WALLA WALLA HS (Vocational) | 48% | 23% | 24% | 5% | 1% | 6% |
| WALLA WALLA (Admin Bldg) | 54% | 32% | 13% | 1% | 0% | 1% |

Walla Walla, Scenario M6.7 earthquake

| Name | None | Slight | Moderate | Extensive | Complete | At least extensive |
|------------------------------------|------|--------|----------|-----------|----------|--------------------|
| BERNEY ELEMENTARY | 0% | 2% | 24% | 59% | 15% | 74% |
| BERNEY ELEMENTARY (Gymnasium) | 0% | 3% | 31% | 56% | 10% | 67% |
| BLUE RIDGE ELEMENTARY | 0% | 4% | 39% | 49% | 8% | 56% |
| EDISON ELEMENTARY | 52% | 38% | 10% | 0% | 0% | 0% |
| GARRISON MIDDLE | 34% | 54% | 12% | 0% | 0% | 0% |
| GREEN PARK ELEMENTARY L (addition) | 2% | 24% | 66% | 9% | 0% | 9% |
| GREEN PARK ELEMENTARY (original) | 1% | 14% | 51% | 30% | 4% | 34% |
| LINCOLN ALTERNATIVE HIGH | 3% | 19% | 53% | 23% | 3% | 26% |
| PAINE CAMPUS | 0% | 16% | 26% | 29% | 28% | 57% |
| PIONEER MIDDLE | 28% | 56% | 16% | 0% | 0% | 0% |
| PROSPECT POINT ELEMENTARY | 48% | 33% | 19% | 1% | 0% | 1% |
| SHARPSTEIN ELEM S (Gym and Lunch) | 42% | 34% | 23% | 1% | 0% | 1% |
| SHARPSTEIN ELEMENTARY | 4% | 21% | 66% | 10% | 0% | 10% |
| WALLA WALLA HS (Academic) | 54% | 30% | 15% | 1% | 0% | 1% |
| WALLA WALLA HS (Auditorium) | 21% | 37% | 40% | 2% | 0% | 2% |
| WALLA WALLA HS (Commons) | 7% | 30% | 50% | 13% | 1% | 14% |
| WALLA WALLA HS (Large Gym) | 54% | 30% | 15% | 1% | 0% | 1% |
| WALLA WALLA HS (Library) | 27% | 36% | 35% | 2% | 0% | 2% |
| WALLA WALLA HS (Music) | 21% | 37% | 40% | 2% | 0% | 2% |
| WALLA WALLA HS (Science) | 54% | 30% | 15% | 1% | 0% | 1% |
| WALLA WALLA HS (Small Gym) | 7% | 30% | 50% | 13% | 1% | 14% |
| WALLA WALLA HS (Vocational) | 27% | 36% | 35% | 2% | 0% | 2% |
| WALLA WALLA ADMIN BUILD. | 28% | 56% | 16% | 0% | 0% | 0% |

In subsequent years, we hope to be able to secure dedicated funding to extend this analysis statewide or at least to school districts prioritized on the basis of this analysis. Alternatively, school districts could be prioritized in order of the amount by which ground shaking hazard has increased in the current building code since enactment of the State Building Code Act of 1974. Based upon the results of this pilot project it is estimated that completing a statewide assessment program using the previously described approach would be roughly \$10-13 million dollars that could be phased over an 8-10 year period. This equates to approximately \$3,500-\$4,500 per public school throughout the state and such an approach could be supported by a combination of federal, state, and local resources.



Table 3. School retrofit projects in Washington since the Nisqually earthquake, February 28, 2001. The total is the total cost of the project, including FEMA, state and local matching funds.

| Project | Cost | Status |
|---|---------------------|--------------------|
| Retrofit of Residence Hall A at The Evergreen State College | \$1,456,463 | Ongoing |
| Retrofit of Library Clock Tower at The Evergreen State College | \$1,055,600 | Ongoing |
| Non-structural retrofit at Burke Museum at the University of Washington | \$949,039 | Nearing completion |
| Retrofits of two dormitories at Pacific Lutheran University | \$2,100,334 | Complete |
| Retrofits of two dormitories at Pacific Lutheran University | \$2,100,334 | Complete |
| Retrofit shop at Lake Washington Technical College | \$72,163 | Complete |
| Retrofit of nine elementary schools in Edmonds | \$6,966,715 | Complete |
| Retrofit of facilities at Clark College in Vancouver | \$1,359,915 | Complete |
| Retrofit of facilities at Clark College in Vancouver | \$1,359,915 | Complete |
| Retrofit of school auditorium/cafeteria in LaConner | \$702,658 | Complete |
| Retrofit of elementary school in Littlerock | \$875,535 | Complete |
| Retrofit of Roy Elementary School near Tacoma | \$555,172 | Complete |
| Total | \$18,998,671 | |

Seismic retrofits of Washington schools since the Nisqually earthquake funded at least in part by FEMA. This methodology provides enough information to support benefit-cost analysis necessary for grant funding as well as nonstructural mitigation that could be part of normal maintenance. We are in discussions with OSPI to develop innovative funding options.